

**FERROELECTRIC TUNGSTEN BRONZE BULK CRYSTALS  
AND EPITAXIAL THIN FILMS FOR  
ELECTRO-OPTIC DEVICE APPLICATIONS**

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↘ broad range of tungsten bronze materials. This indicates that the hypothesis of near-constant higher order stiffness parameters is a good approximation for tetragonal bronze ferroelectrics, thereby allowing the analysis of a very wide range of other bronze compositions. ↗



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## 1.0 SUMMARY AND PROGRESS

Tungsten bronze (T.B.) family crystals have been shown to be useful for a number of device applications, including electro-optic waveguides, photorefractive holography and pyroelectric FPA. The current work reports on the development of good quality (acceptable for device studies)  $\text{Sr}_{1-x}\text{Ba}_x\text{Nb}_2\text{O}_6$ ,  $x = 0.40$  and  $0.50$ , and morphotropic phase boundary compositions. The composition SBN:60 has been used for electro-optic and nonlinear optical applications, while SBN:50 will be developed for pyroelectric FPA applications. Considerable progress has been made in several areas, including the growth of Ce- and Fe-doped SBN:60 crystals. Based on current work, a number of new dopants have also been identified for both photorefractive and pyroelectric studies. This work also includes the continued effort to search for new T.B. systems specifically based on morphotropic phase boundary compositions for photorefractive and transverse pyroelectric FPA applications.

Several doped ( $\text{Ce}^{3+}/\text{Ce}^{4+}$  and  $\text{Fe}^{2+}/\text{Fe}^{3+}$ ) and undoped SBN:60 single crystals have been grown using the Czochralski technique. Optical evaluation shows that Ce-doped crystals have minimum or no striations and are of optical quality, while Fe-doped crystals are highly striated under all growth conditions, and the striations are found difficult to suppress. In the tungsten bronze structure,  $\text{Ce}^{3+}$  and  $\text{Ce}^{4+}$  are expected to occupy the 12- and 9-fold coordinated sites, while  $\text{Fe}^{2+}$  and  $\text{Fe}^{3+}$  ions are expected to occupy 6-fold coordinated sites. Our current results suggest that the existence of striations in SBN:60 crystals depends strongly on the type of dopant and its location in the structure. Since  $\text{Mn}^{2+}$ ,  $\text{Co}^{2+}$  and  $\text{Cr}^{3+}$ , etc., have ionic size and site preferences similar to  $\text{Fe}^{3+}$ , it will be interesting to check their influence on striations in SBN:60 crystals. Ce-doped SBN:60 crystals currently exhibit excellent photorefractive properties with improved sensitivity and speed, indicating possible use for this material in device applications.

Since the composition SBN:50 has a higher Curie temperature (110 - 120°C) and also an excellent figure-of-merit for pyroelectric FPA applications,



a systematic study of this crystal has recently been initiated. This composition is slightly off congruent melting; however, using the current Czochralski technique it has been possible to grow good quality crystals as large as 1 cm in diameter. Efforts are now underway to establish its pyroelectric and dielectric properties for FPA applications.

An extensive discussion of the thermodynamic phenomenology for tungsten bronze crystals is presented in the Appendix along with a tabulation of a number of thermodynamic constants based on current research and other data in the literature. An excellent fit to birefringence polarization data for  $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$  (BNN) is found for the Devonshire form of the Gibbs free-energy expansion, and good agreement is found for a number of thermodynamic constants over a broad range of tungsten bronze materials. This indicates that the hypothesis of near-constant higher order stiffness parameters is a good approximation for tetragonal bronze ferroelectrics, thereby allowing the analysis of a very wide range of other bronze compositions.





## 2.0 DEVELOPMENT OF OPTICAL QUALITY SBN CRYSTALS

### 2.1 Material Growth Techniques

Most of the bronze compositions grown in our laboratory are based on solid solution systems; therefore suitable growth techniques to produce crystals free of optical defects such as striations, scattering centers and twinning must be developed. Striations and other defects are typical problems common to solid solution crystals, and it is often difficult to suppress them completely. However, these problems can be reduced effectively such that the crystals can be useful for optical device studies. The difficulty of this task underscores the criticality of selecting appropriate growth techniques in the present work. At present, three different techniques have been chosen to develop SBN and other bronze crystals. They are as follows:

1. Bulk Single Crystals: Czochralski technique
2. Thin Films: Liquid phase epitaxy (LPE)
3. Strip Crystals: Edge defined film-fed technique

The first two techniques are well established in our current work, and bulk crystals and films of SBN compositions have already been grown. In the present report, the continued growth of striation-free SBN crystals is discussed along with associated growth problems.

### 2.2 Growth Procedure

$\text{Nb}_2\text{O}_5$ ,  $\text{SrCO}_3$ ,  $\text{Fe}_2\text{O}_3$ ,  $\text{CeO}_2$  and  $\text{BaCO}_3$  fine powders have been used as starting materials and have been weighed out in the desired proportions, as summarized in Table 1. The batch mixture is ball-milled in acetone for 20-30 h, and then is poured into a large drying dish. The dried powder is placed in a platinum reaction dish and is calcined at  $1000^\circ\text{C}$  for 10-15 h to eliminate carbonates and any possible carbon from the pyrolytic breakdown of residual acetone. The calcined powder is then ball-milled and refired in an oxygen flow of 2 cfh at  $1400^\circ\text{C}$  for about 4 - 6 h. Phase checks and x-ray lattice constant



Table 1  
Materials for Bulk Single Crystal SBN:60 Growth

Crystal Composition	Starting Materials		Conditions and Remarks
SBN:60	a. $\text{SrCO}_3$	135.08 gms	Congruent melting composition
	b. $\text{BaCO}_3$	115.48 gms	Large crystals can be grown
	c. $\text{Nb}_2\text{O}_5$	398.73 gms	Large electro-optic coefficient ( $r_{33}$ )
	Total wt.	649.26 gms	Melts at 1510°C
	Growth wt.	450.00 gms	Crack-free and optical quality
SBN:60 + $\text{Fe}^{3+}$	a. $\text{SrCO}_3$	135.08 gms	Dielectric and electro-optic coefficient increased
	b. $\text{BaCO}_3$	115.48 gms	Growth of large crystals is possible
	c. $\text{Nb}_2\text{O}_5$	398.73 gms	Enhanced photorefractive properties
	d. $\text{Fe}_2\text{O}_3$	1.98 gms	Crack-free crystals
		to 3.05 gms	
	Total wt.	651.24 gms	
SBN:60 + $\text{Ce}^{3+}$	a. $\text{SrCO}_3$	135.08 gms	Dielectric and electro-optic coefficient improved
	b. $\text{BaCO}_3$	115.48 gms	Growth of large crystals is possible
	c. $\text{Nb}_2\text{O}_5$	398.73 gms	Enhanced photorefractive properties
	d. $\text{CeO}_2$	1.00 gms	Crack-free and optical quality crystals
		to 1.50 gms	
	Total wt.	650.26 gms	
	Growth wt.	450.00 gms	

measurements are made for each batch to ensure the use of a phase-pure bronze composition for crystal growth. A thick-walled platinum crucible of 2 2 in. in dimension is used for this growth, and this container holds roughly 450 g of melt composition.



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### 2.3 Growth of $\text{Sr}_{1-x}\text{Ba}_x\text{Nb}_2\text{O}_6$ , $x = 0.40$ and $0.50$

As summarized in Table 2, we have grown a number of doped and undoped SBN:60 and SBN:50 single crystals of excellent quality using the Czochralski technique. Small amounts of impurities have been shown to have a drastic photorefractive effect in optical applications. According to the current device need, the growth compositions have been modified as follows:

- a. Optical Waveguide (NRL): High optical quality starting materials to avoid photorefractive and striation effects. SBN:60 composition has only been used for this task.
- b. Photorefractive Studies: High optical quality starting materials with specific impurities, e.g., Ce or Fe, in SBN:60.
- c. Pyroelectric Studies: High optical quality starting materials. Main emphasis on the SBN:50 composition.

### 2.4 Growth of Doped SBN:60 Crystals

The main objective of this task is to enhance the photorefractive sensitivity and speed of ferroelectric SBN:60 single crystals using specific impurity species. The current trend in ferroelectric materials indicates that the photorefractive sensitivity of SBN:60 is very large, on the order of  $10^{-3}$  or higher. However, the response time for these crystals is relatively slow when compared with the best known nonferroelectric cubic  $\text{Bi}_{12}\text{SiO}_{20}$  (BSO) crystals, which have a response time typically on the order of 1 ms.

To improve response time and sensitivity, considerable progress has been made using appropriate dopants in materials such as SBN:60,  $\text{KNbO}_3$ ,  $\text{BaTiO}_3$ , and  $\text{LiNbO}_3$ . The most commonly used dopants in these crystals include  $\text{Fe}^{2+}/\text{Fe}^{3+}$ ,  $\text{Ce}^{3+}/\text{Ce}^{4+}$ ,  $\text{Mo}^{4+}/\text{Mo}^{6+}$ , and  $\text{U}^{4+}/\text{U}^{6+}$ . To develop high sensitivity and fast response in tungsten bronze SBN:60 crystals, effort has focussed on the



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Table 2  
Growth of SBN:60 and SBN:50 Crystals

Boule No. 2	Date Grown	Boule wt.	Dip °C	Rotation rpm	Remarks, Observations
185	05/29/84	16.7	1491	5-8	Uncracked
186	06/01/84	34.6	1489	~ 8	Neck nearly defect-free
187	06/06/84	38.3	1491	~ 8	ADC used, uncracked
188	06/12/84	25	1482	5-15	New charge - flat top, heavily defected, cracks 5 nines purity - less color
189*	06/18/84	25.3	1484	~10	Uncracked - appears core-free
190	06/21/84	18.6	1485	10-12	Uncracked - core-free
191	07/10/84	27.8	1485	8-10	Uncracked - had to de-twin
192	07/13/84	14.3	1486	10	One deep twin - cracked along one side
193	07/30/84	27	1480	~12	Minor coring, uncracked
194	08/02/84	38	1485	10	Good ADC, uncracked core-free boule
195*	08/23/84	42.5	1485	~10	1.8-1.9 cm dia, uncracked
196	08/27/84	49	1485	10	2.0 cm dia, uncracked
197	08/30/84	29	1490	10	Uncracked
198	09/11/84	~5	1490	10	Test new load cell (test crystal)
199	09/25/84	29.5	1485	12	Test new crucible support (small boule)
200	09/28/84	52.5	1485	5-10	Small bubble in boule neck ~19 mm dia
201	10/03/84	41	~1485	5-10	Pink color boule, 19 mm di
202	10/05/84	41	~1485	5-10	Pink color, 18 mm dia Minor twinning
203	10/10/84	18	~1485	~10	Pink, uncracked
204	10/18/84	35.7	~1485	5-10	Dark pink, no twins, uncracked
205	10/30/84	~15	~1485	10-15	Wine color, uncracked

\*To NRL



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increase of the space charge field,  $E$ , since the change in refractive index,  $\Delta n$ , is linearly proportional to  $E$  from the relation

$$\Delta n = 1/2 n_1^3 r_{ij} E_j, \quad (2.1)$$

where  $r$  is the electro-optic coefficient.

Table 3 summarizes the various dopants selected in the present study, their valence states, and their anticipated site preferences in the tungsten bronze structure. Since the role of  $\text{Fe}^{2+}/\text{Fe}^{3+}$  and  $\text{Ce}^{3+}/\text{Ce}^{4+}$  has been widely studied in various ferroelectric crystals, the present work has concentrated on these dopants. The growth and feasibility of SBN:60 crystals doped with these ions have been discussed in our previous report. Since then, considerable progress has been made to improve the quality of these crystals for potential use in photorefractive device applications.

Table 3  
Role of Dopants in SBN:60

Dopant	Site Preference				Configuration	Basic	°C	Dielectric Constant	Comments
	15-fold	12-fold	9-fold	6-fold					
$\text{Ce}^{3+}$	-	$\text{Ce}^{3+}$	-	-	$4f^1 5s^2 5p^6$	$2F_{5/2}$	Reduced	Increased	Large Crystals
$\text{Ce}^{4+}$	-	$\text{Ce}^{4+}$	$\text{Ce}^{4+}$	$\text{Ce}^{4+}$	-	-	Reduced	Increased	Large Crystals
$\text{Fe}^{3+}$	-	-	-	$\text{Fe}^{4+}$	$3d^5$	$6S_{5/2}$	Reduced	Increased	Large Crystals
$\text{Fe}^{2+}$	-	-	$\text{Fe}^{2+}$	$\text{Fe}^{2+}$	$3d^6$	$5D_4$	-	Increased	Large Crystals
$\text{Cr}^{3+}$	-	-	-	$\text{Cr}^{3+}$	$3d^3$	$4F_{3/2}$	-	-	-
$\text{Mn}^{2+}$	-	-	$\text{Mn}^{2+}$	$\text{Mn}^{2+}$	$3d^5$	$6S_{5/2}$	-	-	-
$\text{Mn}^{3+}$	-	-	-	$\text{Mn}^{3+}$	$3d^4$	$5D_0$	-	-	-
$\text{Nb}^{4+*}$							Reduced	Increased	Large Crystals

\* $\text{Nb}^{5+}$  reduces to  $\text{Nb}^{4+}$  at high temperature.



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Recently, we successfully demonstrated the growth of Ce- and Fe-doped SBN:60 single crystals as part of our effort to study in detail the role of these ions in photorefractive device applications. As shown in Fig. 1 approximately 1 to 2 cm diameter Ce- and Fe-doped SBN:60 crystals have been grown along the (001) direction using the Czochralski technique. Doping of SBN:60 with Fe, and Fe and Ce together, has not been done previously, and Fe is expected to produce interesting results, as it has been observed to do in other ferroelectric crystals such as  $\text{LiNbO}_3$  and  $\text{KNbO}_3$ .

Ce-doped SBN:60 crystals show minimum or no striations, and the crystals are of optical quality, while Fe-doped crystals are highly striated under all growth conditions, and the striations are found difficult to suppress. In the tungsten bronze structure,  $\text{Ce}^{3+}$  and  $\text{Ce}^{4+}$  are expected to occupy the 12- and 9-fold coordinated sites, while  $\text{Fe}^{2+}$  and  $\text{Fe}^{3+}$  ions are expected to occupy 6-fold coordinated sites. Our results suggest that the existence of striations in SBN:60 crystals depends strongly on the type of dopant and its location in the structure. Since  $\text{Mn}^{2+}/\text{Mn}^{3+}$ ,  $\text{Co}^{2+}/\text{Co}^{3+}$ ,  $\text{Ti}^{3+}/\text{Ti}^{4+}$ , etc., have ionic size and site preference similar to  $\text{Fe}^{3+}$ , it will be interesting to check their influence on striations in SBN:60 crystals.

The development of striation-free Ce-doped SBN:60 crystals makes possible the evaluation of the photorefractive properties, specifically sensitivity and speed. Typical  $6 \times 6 \times 6$  mm size cubes have been supplied for examination, and two- and four-wave mixing techniques are being used. These measurements are being made at Caltech and other laboratories, and will be reinvestigated as better quality crystals become available. Table 4 summarizes the proposed goals set and results obtained to date for SBN:60 crystals. In agreement with the results reported by Megumi et al,<sup>1</sup> the present crystals show the typical Ce broad absorption band around  $0.50 \mu\text{m}$ , and this band remains unchanged from one sample to another.



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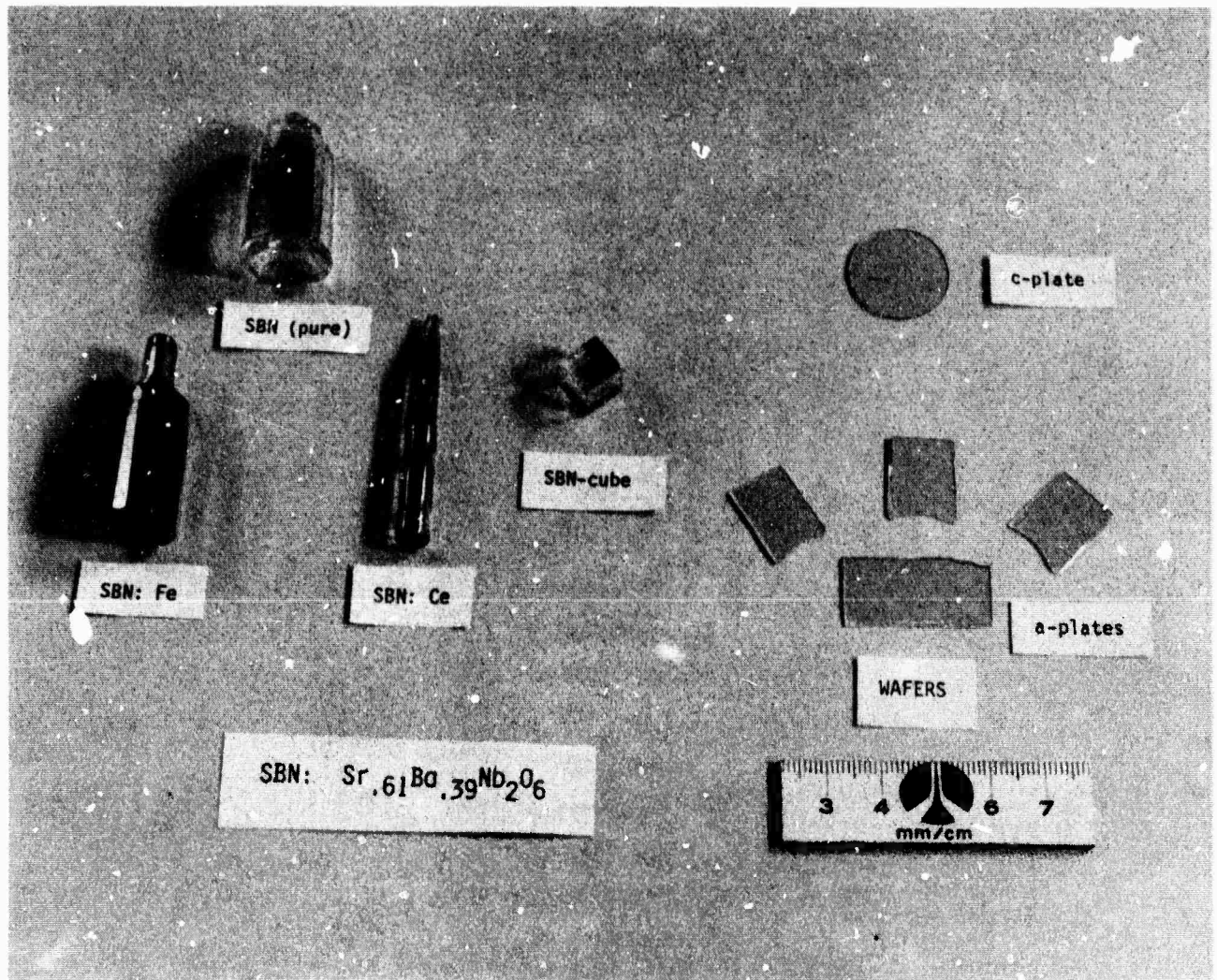


Fig. 1 Doped and undoped SBN:61 single crystals grown  
at the Rockwell International Science Center.



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Table 4  
Goals for Photorefractive Studies and Current Results

Desired Properties	Observed Properties
1. Response time $\sim 1$ ms	1. Response time achieved $< 100$ ms
2. Sensitivity $\sim 10^{-4}$ to $10^{-5}$ $\text{cm}^2/\text{J}$	2. Sensitivity achieved $\sim 10^{-3}$ $\text{cm}^2/\text{J}$
3. Coupling coefficient $\sim 1$ $\text{cm}^{-2}$	3. Coupling coefficient achieved $\sim 11$ $\text{cm}^{-1}$
4. Large size, optical quality crystals	4. Large size (2.5 cm in diameter) and striation-free SBN:60 and $\text{Ce}^{3+}$ -doped SBN:60 crystals are available
5. Large electro-optic coefficient necessary	5. Electro-optic coefficient enhanced for $\text{Fe}^{3+}$ and $\text{Ce}^{3+}$ additions

A useful evaluation method for the photorefractive sensitivity of electro-optic crystals is the sensitivity,  $S$ , defined as the index change per absorbed energy density,

$$S = \frac{\Delta n}{\Delta W_{\text{abs}}} \quad (2.2)$$

For 0.1 wt% Ce-doped crystals, this sensitivity was measured to be  $6.5 \times 10^{-3}$   $\text{cm}^2/\text{J}$ . This value is in close agreement with the value reported by Megumi et al.,<sup>1</sup> and exceeds that of Fe-doped  $\text{LiNbO}_3$  and  $\text{Mo}^{4+}$  and  $\text{Fe}^{3+}$  doped  $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$  by more than two orders of magnitude. For this addition, the response time also changed, becoming faster ( $\sim 80$  to  $100$  msec) compared to undoped crystals ( $\sim 100$  msec). These are considered to be significant improvements, and although details regarding the photorefractive mechanisms are not yet known with certainty, it appears that one can improve both the response time and sensitivity with suitable dopants. Fe-doped crystals also show similar improvements; however, the estimation of precise values has been difficult due to marginal crystal quality. Efforts are now underway to investigate the striation problems associated with Fe-doped SBN:60 crystals.

The improvement in photorefractive characteristics needs to be related to the possible roles of these impurities. In the ideal picture, one needs both





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a donor of electrons and an acceptor to enhance the space charge field  $E_1$ . These might be  $Ce^{3+}$  and  $Ce^{4+}$ ,  $Fe^{2+}$  and  $Fe^{3+}$ ,  $Ce^{3+}$  and  $Fe^{3+}$ , or combinations of these with  $Nb^{4+}$  and various vacancies in the SBN:60 structure. The current results clearly indicate that the addition of Ce and Fe dopants enhances the photorefractive properties; however, the ratio of the various charge states of  $Ce^{3+}/Ce^{4+}$  or  $Fe^{2+}/Fe^{3+}$  has not yet been established. Because  $Ce^{3+}$  (or  $Fe^{3+}$ ) is stable at the growth temperature, there exist several possibilities for the species which form charge traps, as shown in Table 5. In the present case, the tendency of  $Nb^{5+}$  to reduce to  $Nb^{4+}$  provides the possibility of donor states. Since the preferred state of Ce at the growth temperature is  $Ce^{3+}$ , a donor, there is some question concerning the identity of the acceptor level in Ce-doped crystals. The observed tendency of  $Nb^{5+}$  to reduce at the growth temperature may encourage the formation of vacancies, which would act as either donors or acceptors. Currently, we are using optical and Mössbauer spectroscopy to identify the donor and acceptor species in these crystals. Once this is accomplished, it should be possible to control both the sensitivity and speed in a more effective manner.

Table 5  
Valance States of Dopants in SBN

Dopant	Crystallographic Sites				Donor	Acceptor	Stable States*
	15-	12-	9-	6-			
$Ce^{+}$	-	$Ce^{3+}$	$Ce^{4+}$	--	$Ce^{3+}$	$Ce^{4+}$	$Ce^{3+}$
Ce and Nb	-	$Ce^{3+}$	$Ce^{4+}$	$Nb^{4+}$	$Ce^{3+}$ , $Nb^{4+}$	$Ce^{4+}$	$Ce^{3+}$ , $Nb^{5+}$
Ce	-	$Ce^{3+}$	--	--	$Ce^{3+}$	Cation Vac.	$Ce^{3+}$
Fe	-	--	--	$Fe^{2+}$ , $Fe^{3+}$	$Fe^{2+}$	$Fe^{3+}$	$Fe^{3+}$
Fe, Nb	-	--	--	$Fe^{3+}$ , $Nb^{4+}$	$Nb^{4+}$	$Fe^{3+}$	$Fe^{3+}$ , $Nb^{5+}$
Fe	-	--	--	$Fe^{3+}$	Cation Vac.	$Fe^{3+}$	$Fe^{3+}$
Ce, Fe	-	$Ce^{3+}$	--	$Fe^{3+}$	$Ce^{3+}$	$Fe^{3+}$	$Ce^{3+}$

\*Valance state at growth temperature,  
Vac. - Vacancy



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The improvement in photorefractive properties obtained by doping SBN:60 crystals presents a unique opportunity to study new device concepts. At the same time, these studies are providing the basis for understanding the photorefractive mechanism responsible for these improvements, as well as guiding the search for new classes of electro-optic materials. For the next six months the following aspects of SBN crystal growth will be studied:

- Establish the valence states of Ce in SBN:60 single crystals.
- Establish whether any free  $\text{Nb}^{4+}$  is present in SBN:60 crystals and its effect on photorefractive properties.
- Improve the current growth technique to suppress the striations present in Fe-doped SBN:60 crystals. Also, establish the concentration at which striations appear.
- Identify another suitable dopant which will occupy the 6- or 9-fold coordinated sites, e.g.,  $\text{Cr}^{3+}/\text{Fe}^{3+}$ ,  $\text{Co}^{2+}/\text{Co}^{3+}$ ,  $\text{Ti}^{3+}/\text{Ti}^{4+}$ , or other cations.
- Establish the ferroelectric and electro-optic properties with respect to new dopants and evaluate their potential suitability in photorefractive applications.

## 2.5 SBN:50 Crystals for Pyroelectric Studies

The development of doped or undoped  $\text{Sr}_{1-x}\text{Ba}_x\text{Nb}_2\text{O}_6$ ,  $x = 0.50$ , single crystals for pyroelectric focal plane array (FPA) applications is a new task under this contract for the 1985-1987 period. Although contract funding was not available at the time when this work was initiated, we began to study the factors that influence the figure-of-merit for this application. At the present time, the figure-of-merit for a FPA is defined as  $p/\sqrt{\epsilon}$ , where  $p$  is the pyroelectric coefficient and  $\epsilon$  is the dielectric constant, and this value is significantly higher for SBN:50 crystals as compared to many other ferroelectric crystals, as listed in Table 6.



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Table 6  
Leading Pyroelectric Materials

Crystal Composition	$T_c$ (°C)	Dielectric Constant at 23°C	Pyroelectric Coefficient $\times 10^{-10}$ c/cm <sup>-2</sup> K <sup>-1</sup>	Figure-of-Merit	
				$P/\epsilon$	$P/\sqrt{\epsilon}$
TGS	49	28	310	11.07	58.58
TGS:P <sup>5+</sup> *	50	-	-	-	-
LiTaO <sub>3</sub>	660	49	170	3.47	24.28
SBN:60	75	500	850	1.82	38.01
SBN:50	128	300	680	2.28	39.26
SBN:50, 0.5% La <sup>3+</sup>	106	485	1562	3.22	70.92
BSKNN	208	120	485	4.04	44.27
Pb <sub>5</sub> Ge <sub>3</sub> O <sub>11</sub>	152	36	110	3.065	18.33

\*Work is in progress to obtain optimum dopant concentration.

Based on the currently accepted figure-of-merit, clearly for the longitudinal FPA applications, it is important to maintain a high pyroelectric coefficient and a sufficiently low dielectric constant. In the case of SBN:50, the dielectric constant is relatively low; however, a crystal chemical approach is being used to study suitable dopants that will maintain a high pyroelectric coefficient and further reduce the dielectric constant. We have examined the role of various ions in SBN:50 using ceramic samples, and have found that non-3d or 4f ions (e.g., La<sup>3+</sup>) are suitable to enhance the pyroelectric figure-of-merit, while other ions are unsuitable since they increase the dielectric losses. Table 7 summarizes the results of addition of various ions in different crystallographic sites and their influence on the pyroelectric figure-of-merit.



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Table 7  
Effect of Dopants in SBN Crystals

Crystallographic Site							
Dopant	15-Fold	12-Fold	9-Fold	6-Fold	P	$\epsilon$	Tan $\delta$
$\text{La}^{3+}$	$\text{La}^{3+}$	$\text{La}^{3+}$	--	--	Increased	Increased	--
$\text{Ca}^{2+}$	--	$\text{Ca}^{2+}$	--	--	Increased	Increased	Reduced
$\text{Eu}^{3+}$ , $\text{Sm}^{3+}$	$\text{Eu}^{2+}$ , $\text{Sm}^{2+}$	$\text{Eu}^{3+}$ , $\text{Sm}^{3+}$	--	--	Increased	Increased	Increased
$\text{K}^+$ , $\text{Ti}^{4+}$	$\text{K}^+$	$\text{K}^+$	--	$\text{Ti}^{4+}$	--	Reduced	Reduced
$\text{Fe}^{3+}$ , $\text{Ce}^{3+}$	--	$\text{Ce}^{3+}$	--	$\text{Fe}^{2+/3+}$	Increased	Increased	Increased

Since the addition of  $\text{La}^{3+}$  and  $\text{Ca}^{2+}$  favors the enhancement of the pyroelectric figure-of-merit, the growth of  $\text{La}^{3+}$ -doped SBN:50 compositions has been initiated. The substitution of  $\text{La}^{3+}$  in SBN:50 has been studied earlier by Liu et al.,<sup>2</sup> and they were successful in growing small crystals, typically 0.5 to 1.0 cm in diameter. At Rockwell we have been successful in developing excellent quality  $\text{La}^{3+}$ -doped SBN:50 crystals up to 1.7 cm in diameter. This is a significant achievement, and we plan to develop still larger crystals for pyroelectric studies. We will continue to develop the growth technique for this composition during the next six months, and we plan also to evaluate its properties with respect to FPA device requirements.



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### 3.0 THE PHOTOREFRACTIVE EFFECT IN UNDOPE AND DOPED SBN:60

The photorefractive effect in strontium barium niobate (SBN) has now been studied both experimentally and theoretically at Caltech. In particular, we have demonstrated that the introduction of cerium into SBN has resulted in a crystal with a significantly greater photorefractive response.<sup>3</sup> To explain these results, the band transport model for SBN was presented.<sup>4</sup> This theoretical model addressed two-wave mixing in SBN on a microscopic level. This phenomenon is frequently used in the characterization of photorefractive materials<sup>5</sup> and is, therefore, described below.

Consider the two-wave mixing experiment shown in Fig. 2. Beams 1 and 2 are plane waves which intersect in the crystal and thus form an intensity interference pattern. Charge is excited by this periodic intensity distribution into the conduction band, where it migrates under the influence of diffusion and drift in the internal electric field, and then preferentially recombines with traps in regions of low irradiance. A periodic space charge which modulates the refractive index via the electro-optic effect is thus created. This index grating, being out of phase with the intensity distribution, introduces an asymmetry that allows one beam to be amplified by constructive interference with light scattered by the grating, while the other beam is attenuated by destructive interference with diffracted light. This process is shown graphically in Fig. 3.

Mathematically, this two-beam coupling may be described in the steady-state as follows:

$$\frac{dI_1}{d\xi} = -\Gamma \frac{I_1 I_2}{I_1 + I_2} - \alpha I_1 \quad (3.1)$$

$$\frac{dI_2}{d\xi} = \Gamma \frac{I_1 I_2}{I_1 + I_2} - \alpha I_2 \quad (3.2)$$



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where  $I_1, I_2$  are the intensities of beams 1 and 2 inside the crystal respectively,  $\Gamma$  is the two-beam coupling coefficient,  $\alpha$  is the absorption coefficient and  $\xi \equiv z/\cos\theta_1$  where  $0 < \xi < l \equiv d/\cos\theta_1$ . The transient behavior is modeled by the following:

$$I_i(\xi; t) = (1 - e^{-t/\tau}) I_i(\xi; t \rightarrow \infty) + e^{-t/\tau} I_i(\xi; t=0), \quad i=1,2 \quad (3.3)$$

where  $\tau$  is a characteristic time constant and

$$I_i(\xi; t \rightarrow \infty) \equiv I_i(\xi).$$

The solutions of the above coupled wave equations are

$$I_1(l) = \frac{[I_1(0) + I_2(0)]e^{-\alpha l}}{1 + \frac{I_2(0)}{I_1(0)} e^{-\Gamma l}} \quad (3.4)$$

$$I_2(l) = \frac{[I_1(0) + I_2(0)]e^{-\alpha l}}{1 + \frac{I_1(0)}{I_2(0)} e^{-\Gamma l}} \quad (3.5)$$

By measuring the four intensities  $I_1(0)$ ,  $I_2(l)$ , and  $I_2(l)$ , both in the steady-state and as a function of time, the two-beam coupling coefficient  $\Gamma$  and the response time  $\tau$  can, therefore, be obtained from the above equations.

However, both  $\Gamma$  and  $\tau$  can be derived from first principles using the band transport model.<sup>4</sup> Solutions to the photorefractive equations developed most fully by Kuhtarev<sup>6-8</sup> show that  $\Gamma$  and  $\tau$  can be represented functionally as follows:

$$\Gamma = \Gamma(k_g, E_0, \lambda, T; r, N_D, N_A, \epsilon, n)$$

$$\tau = \tau(k_g, E_0, \lambda, T, I_0; s, \gamma_R, \mu, N_D, N_A, \epsilon)$$



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where the experimentally controlled variables are

- $k_g$  = grating wave number
- $E_0$  = applied field (normal to grating planes)
- $\lambda$  = wavelength of incident light
- $T$  = temperature
- $I_0$  = total irradiance

while the material parameters are

- $r$  = effective electro-optic coefficient
- $s$  = photoionization cross-section
- $\gamma_R$  = two-body recombination rate
- $\mu$  = mobility
- $N_D$  = number of donors under dark conditions
- $N_A$  = number of traps under dark conditions
- $\epsilon$  = static dielectric constant
- $n$  = background refractive index.

These equations were applied to cerium doped SBN in earlier work. Specifically, the sample contained  $10^{19} \text{ cm}^{-3}$  cerium atoms which resulted in an as-grown crystal with the following photorefractive parameters:

$$\begin{aligned}\Gamma &= 11 \text{ cm}^{-1} \\ \tau_e &= 0.10 \text{ s} \\ \alpha &= 1.8 \text{ cm}^{-1}\end{aligned}$$

at

$$\begin{aligned}I_0 &= 1 \text{ W/cm}^2 \\ T &= 298 \text{ K} \\ \lambda &= 0.5145 \text{ } \mu\text{m} \\ E_0 &= 0 \text{ V/cm} \\ \lambda_g &= 5 \text{ } \mu\text{m}\end{aligned}$$



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Variations in  $\Gamma$  and  $\tau$  about this operating point are shown in Figs. 4 to 10. With no applied field, Fig. 4 indicates that  $\Gamma$  should be greater than  $1 \text{ cm}^{-1}$  for all practical values of  $\lambda_g$ , while the application of an electric field of 2 kV/cm ought to increase the coupling coefficient to  $35 \text{ cm}^{-1}$  at  $\lambda_g = 5 \mu\text{m}$ , as shown in Fig. 5. Such a large response would then make even very thin samples of SBN:Ce useful photorefractive media. However, in practice, these large values of  $\Gamma$  are not easily obtainable. As an electric field is applied to the crystal, induced stresses deform the material and the incident beams are distorted. Therefore, we conclude that the application of an electric field to the crystal in order to control its two-beam coupling coefficient is of limited use at this point.

Another manner in which  $\Gamma$  can be modified was suggested in Ref. (4). By varying the trap density  $N_A$  with reduction and oxidation treatments, one should be able to control  $\Gamma$  as shown in Fig. 6. Although the exact number density of traps is difficult to measure, we have indeed been able to change the two-beam coupling coefficient from less than  $0.1 \text{ cm}^{-1}$  to  $15 \text{ cm}^{-1}$  by heating the crystal in atmospheres with different oxygen partial pressures. However, the predicted variation of response time with trap density, which is shown in Fig. 7, has yet to be observed in SBN:Ce. Although  $\Gamma$  decreases as expected when the crystal is heated in a reducing atmosphere, the time constant remains unchanged at a typical value of 100 msec at  $1 \text{ W/cm}^2$  irradiance. This unexpected and currently unexplained result has complicated our efforts at producing a cerium doped SBN photorefractive crystal with 1 millisecond response time, since heat treatment was proposed as a method of achieving this goal.<sup>4</sup> Therefore, other techniques may need to be invoked to obtain the desired speed of response.

Figures 8, 9 and 10 show how the response time  $\tau$  is affected with changes in the mobility  $\mu$ , the two-beam recombination rate  $\gamma_R$ , and the photoionization cross-section  $S$ , respectively. Since  $\mu$  is predominantly an intrinsic quantity of the host crystal, little can be done to increase its value. However,  $S$  and  $\gamma_R$  are extrinsic parameters which can be varied by the selection of different dopants. By choosing a dopant with either a larger photoionization cross-section or a smaller two-body recombination rate coefficient than is presently obtained with cerium, the resulting doped sample of SBN should then





possess a shorter response time. The selection of such a dopant, unfortunately, is a nontrivial task.

Consider Table 8 which shows the results of an elemental analysis by nuclear activation of undoped and cerium doped SBN. Since undoped SBN is photorefractive<sup>3</sup> while containing only trace quantities of cerium, we must conclude that cerium is not the only photorefractive species for SBN. In fact, Table 8 indicates that significant amounts of Fe, Ni, Mo and Ta impurities are present in the undoped SBN crystal; Fe and Ni, for example, are known to be effective photorefractive centers in  $\text{LiNbO}_3$ .<sup>9</sup> Although iron has already been used as a dopant for SBN, the resulting crystals are optically imperfect. Therefore, we suggest that not only should the development of iron and cerium-doped SBN continue, but that crystals doped with other impurities, which may prove to have better values of  $\gamma_R$  and  $S$ , should also be investigated.

The growth of SBN with different dopants is a method we now suggest as a means of improving the response time. Since our last report, the reduction of cerium doped SBN was accomplished, but with little effect on  $\tau$ . However, this treatment was shown to vary the two-beam coupling coefficient considerably. The increases in  $\Gamma$  with the application of an electric field were marred by the unexpected distortions of the crystal induced by the field. Finally, the growth of SBN with varying concentrations of cerium proved that optically excellent samples of photorefractive SBN:Ce can now be readily produced.

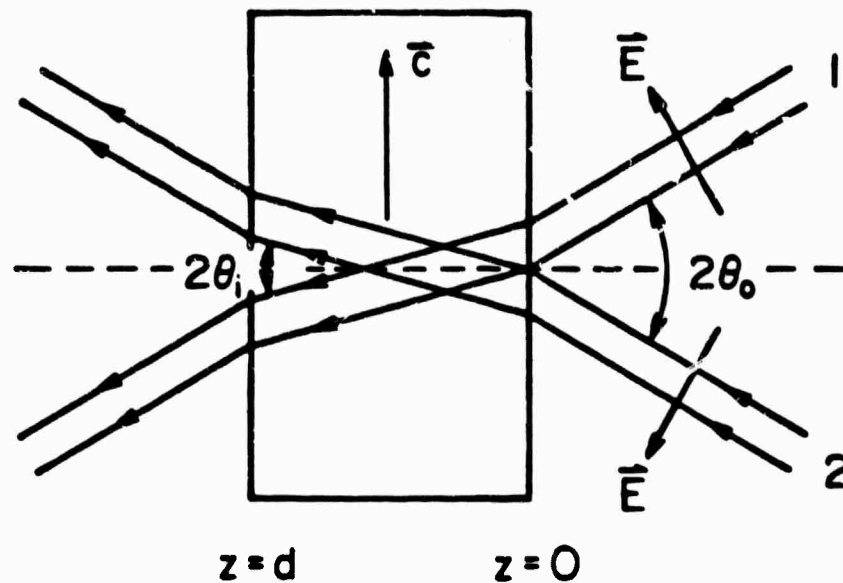


Fig. 2 Experimental setup for two-beam coupling experiments.

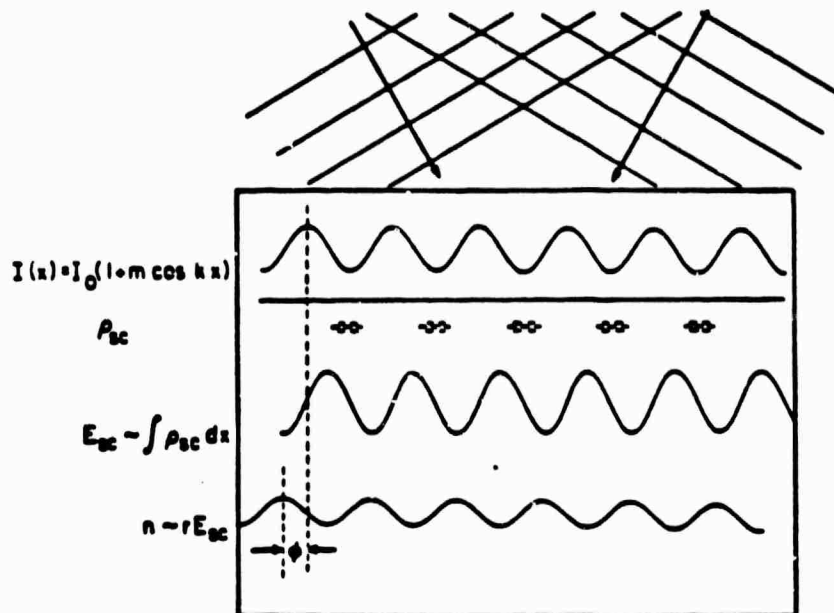


Fig. 3 The photorefractive mechanism.

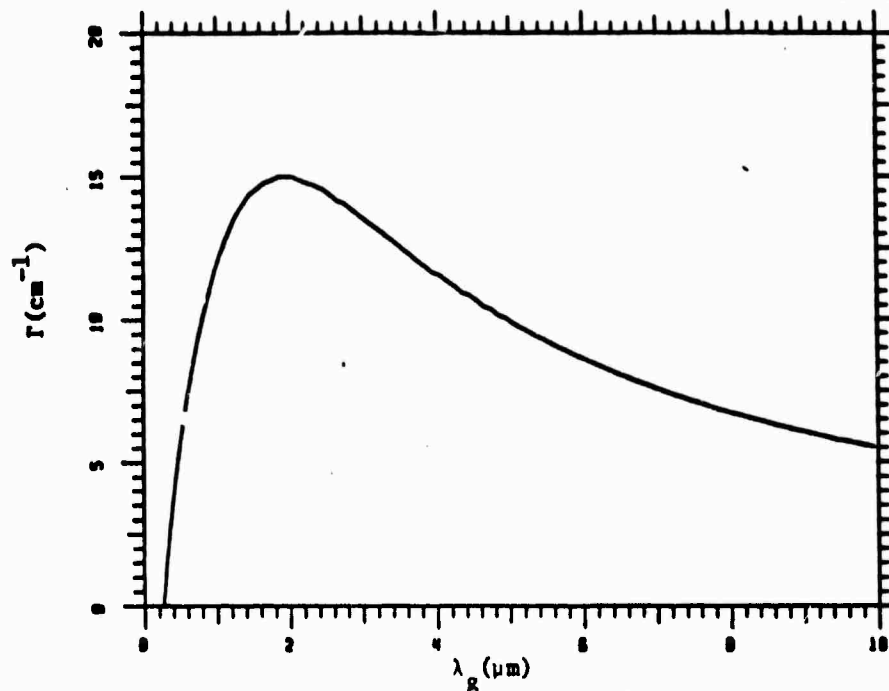


Fig. 4 Coupling coefficient vs grating wavelength for  $E_0 = 0$  V/cm.

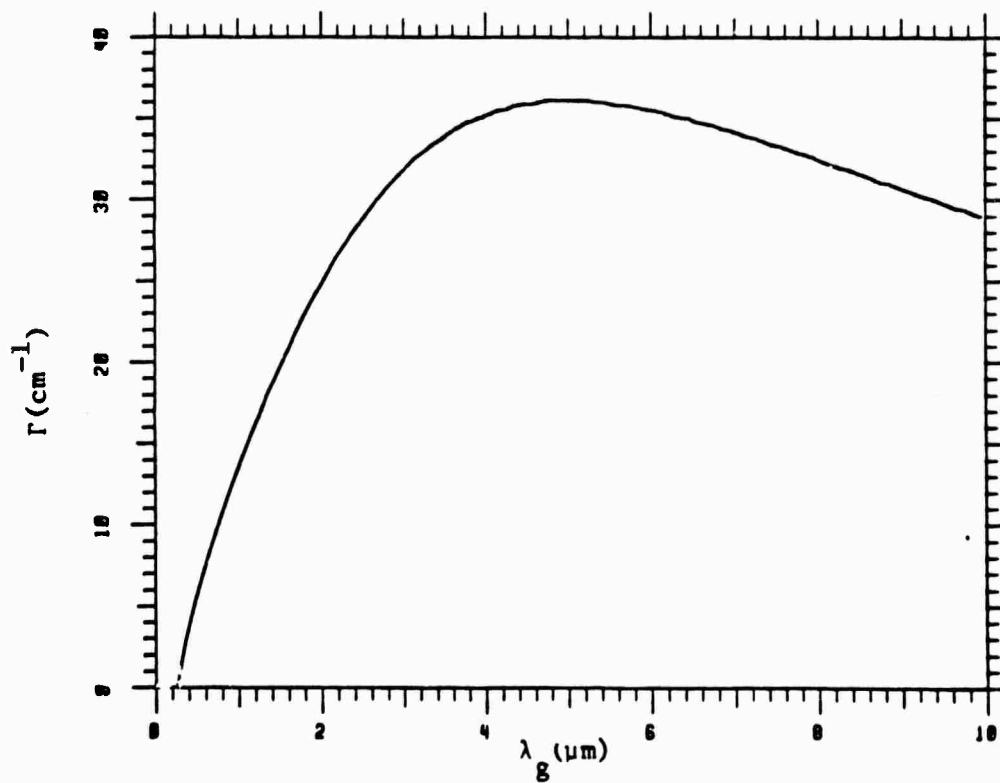


Fig. 5 Coupling coefficient vs grating wavelength for  $E_0 = 2$  kV/cm.

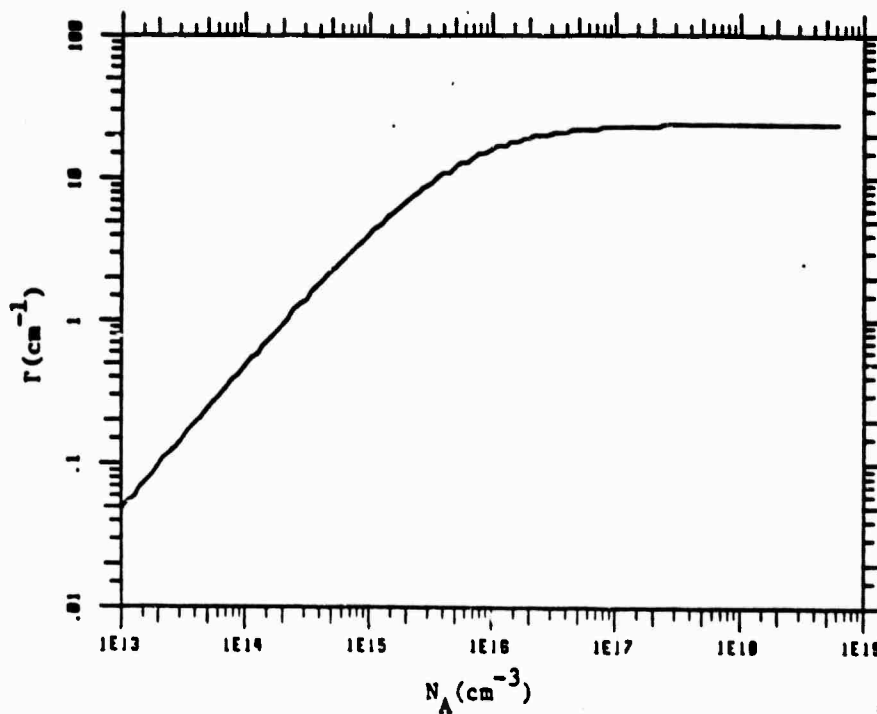


Fig. 6 Coupling coefficient vs acceptor trap density.

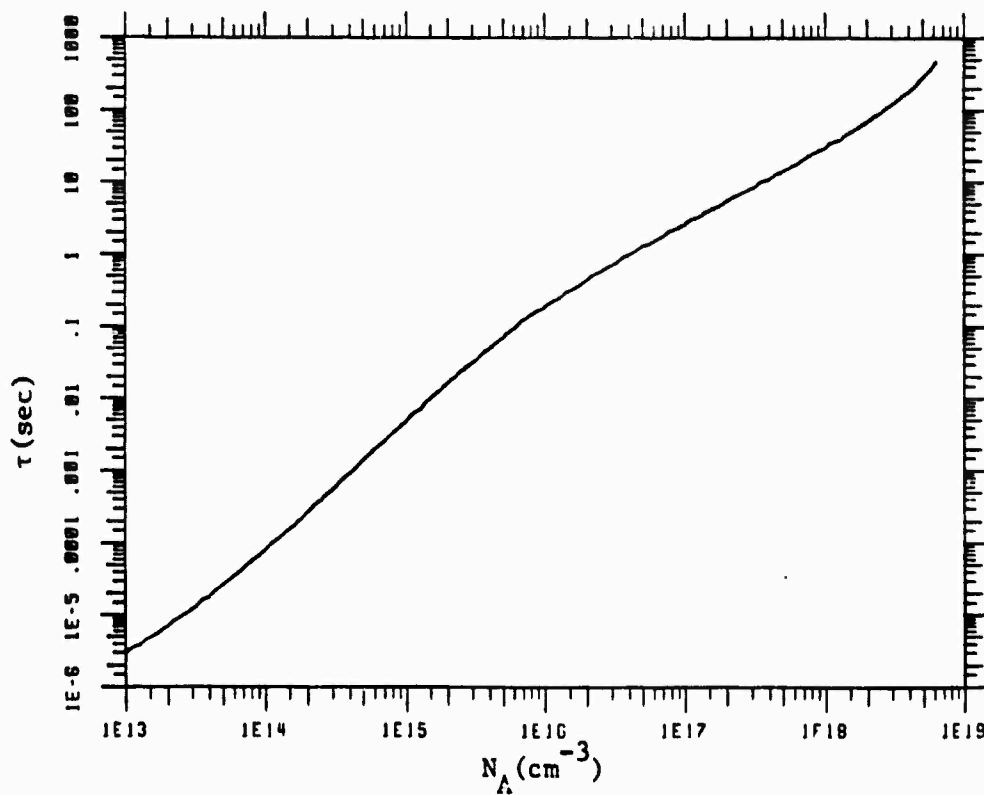


Fig. 7 Response time vs. acceptor trap density.

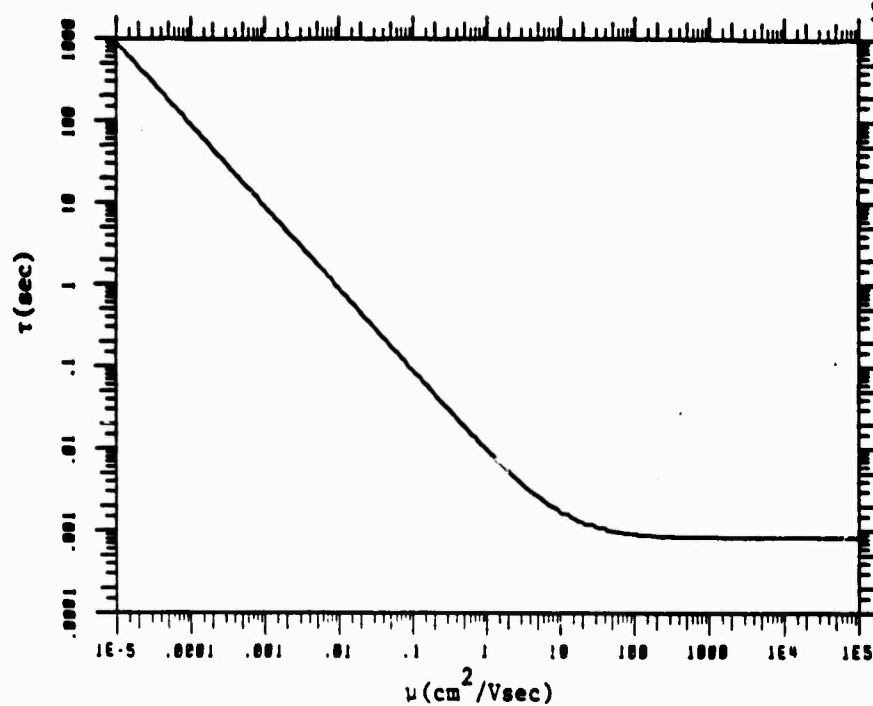


Fig. 8 Response time vs electron mobility.

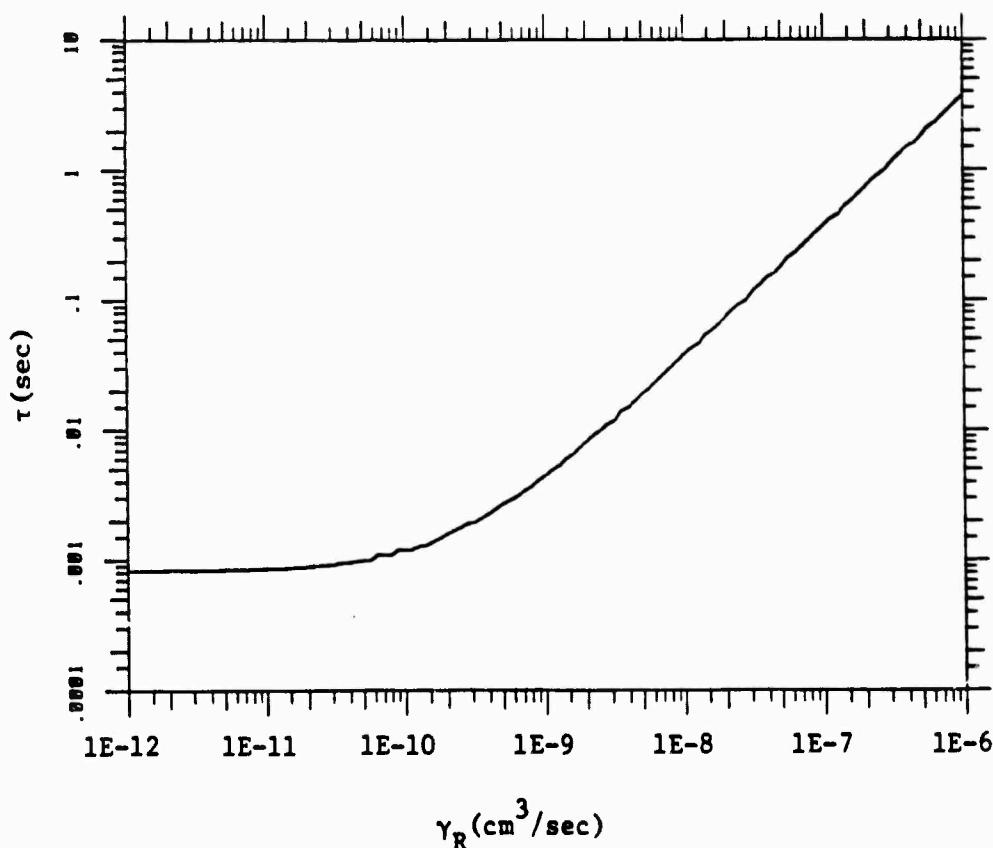


Fig. 9 Response time vs two-body recombination rate coefficient.



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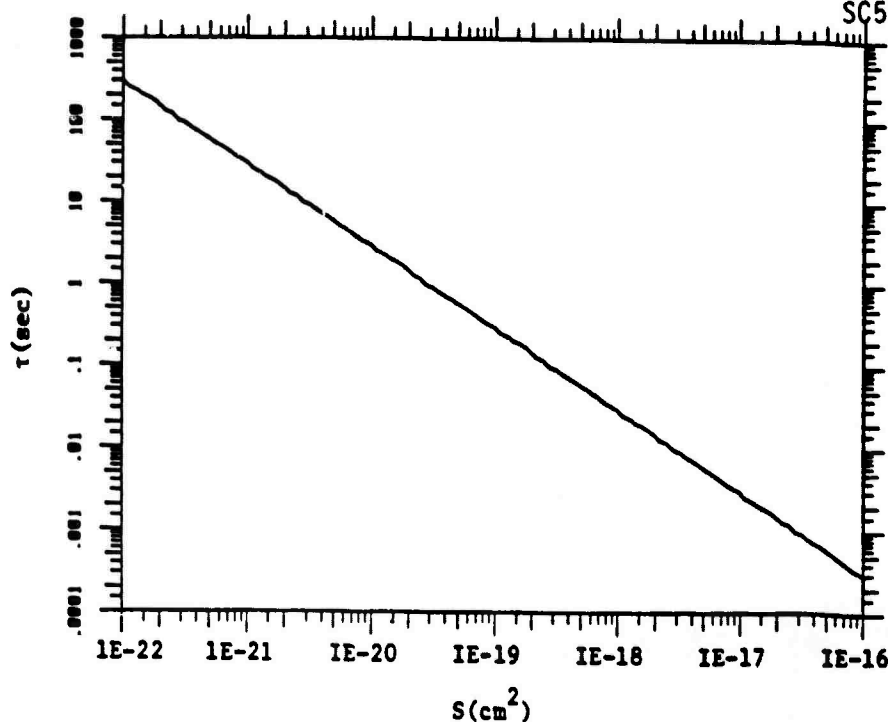


Fig. 10 Response time vs photoionization cross-section.

Table 8

Elemental Analysis by Weight of SBN and SBN:Ce

ELEMENT & UNITS	SBN**	SBN:CE**
U PPM	<0.1	<0.1
TM PPM	<0.3	<0.2
NA PPM	30	<30
SC PPM	0.04	0.03
CR PPM	<5.0	<5.0
FE %	0.029	0.014
CO PPM	0.3	0.3
NI PPM	90	90
IN PPM	7	9
AS PPM	<1	<1
SE PPM	<5.0	<5.0
BR PPM	<0.5	<0.5
MO PPM	11	4
SB PPM	0.5	0.5
CS PPM	<0.2	<0.2
BA PPM	160000	150000
LA PPM	0.2	1.0
HF PPM	<0.2	<0.2
TA PPM	12	13
W PPM	<3	1
AU PPM	<5	5
CE PPM	<1	47
NO PPM	INTERFER	INTERFER
SM PPM	0.01	0.32
SU PPM	0.07	0.10
TB PPM	<0.1	<0.1
VB PPM	<0.05	0.05
LU PPM	<0.01	<0.01
SR PPM	140000	135000
RB PPM	<5	<5



#### 4.0 FUTURE PLANNED WORK

- Further refine and evaluate the growth of high purity SBN:50 and SBN:60 single crystals.
- Continue development of Fe- and Ce-doped SBN:60, and attempt to establish the dopant valence states using optical spectroscopy and other analytical techniques.
- Investigate the dielectric and optical properties of SBN:60 doped with other cations such as  $\text{Cr}^{3+}$ ,  $\text{Co}^{2+}/\text{Co}^{3+}$ , etc.
- Establish the pyroelectric figure-of-merit for tungsten bronze ferroelectric compositions using the crystal chemical approach.
- Continue measurement of the E-O coefficients for near-morphotropic single crystal PBN.
- Continue to evaluate photorefractive properties, specifically sensitivity and speed, using two- and four-wave mixing techniques.



## 5.0 PUBLICATIONS AND PRESENTATIONS

### 5.1 Publications

1. R.R. Neurgaonkar, W.K. Cory and J.R. Oliver, "Growth and Applications of Ferroelectric Tungsten Bronze Family Crystals," *Ferroelectrics* 51, 3 (1983).
2. R.R. Neurgaonkar, J.R. Oliver and L.E. Cross, "Ferroelectric Properties of Tetragonal Tungsten Bronze Single Crystals," *Ferroelectrics* 56, 31 (1984).
3. T.R. Shrout, L.E. Cross and D.A. Hukin, "Ferroelectric Properties of Tungsten Bronze Lead Barium Niobate (PBN) Single Crystals."
4. R.R. Neurgaonkar and L.E. Cross, "Piezoelectric Tungsten Bronze Crystals for SAW Applications," submitted to *Mat. Res. Bull.*
5. R.R. Neurgaonkar, W.K. Cory and J.R. Oliver, "Growth and Applications of T-B Family Crystals," accepted *Proc. Southwest Optics Symposium*.
6. R.R. Neurgaonkar, W.K. Cory and J.R. Oliver, "Growth of Tungsten Bronze Ferroelectric KLN Crystals," submitted to *J. Cryst. Growth*.

### 5.2 Presentations

1. R.R. Neurgaonkar, W.K. Cory and J.R. Oliver, "Growth and Applications of Tungsten Bronze Family Crystals," presented at the 1983 IEEE Int. Symp. on Applications of Ferroelectrics, June 1-3, 1983, Gaithersburg, MD.
2. R.R. Neurgaonkar, J.R. Oliver and L.E. Cross, "Growth and Application of Ferroelectric Tungsten Bronze Family Crystals," presented at the 5th European Meeting on Ferroelectrics, Sept. 26-30, 1983, Benalmadena, Spain.
3. T.R. Shrout, H.C. Chen and L.E. Cross, "Dielectric and Piezoelectric Properties of Tungsten Bronze Lead Barium Niobate ( $\text{Pb}_{1-x}\text{Ba}_x\text{Nb}_2\text{O}_6$ ) Single Crystals," presented at the 5th European Meeting on Ferroelectrics, Sept. 26-30, 1983, Benalmadena, Spain.
4. J.R. Oliver and R.R. Neurgaonkar, "Ferroelectric Solid Solutions Based on the Tungsten Bronze Structure," presented at the 86th Annual Meeting of the Am. Ceram. Soc., April 30-18, 1984, Pittsburgh, PA (invited paper).
5. J.R. Oliver and R.R. Neurgaonkar, "Morphotropic Tungsten Bronze Solid Solutions," presented at the 37th Pacific Coast Regional Meeting of the Am. Ceram. Soc., October 28-31, 1984, San Francisco, CA.





6. R.R. Neurgaonkar, W.K. Cory and J.R. Oliver, "Ferroelectric Tetragonal Tungsten Bronze Crystals for Optoelectronic Applications," presented at the 37th Pacific Coast Regional Meeting of the Am. Ceram. Soc., October 28-31, 1984, San Francisco, CA.
7. R.R. Neurgaonkar, W.K. Cory and J.R. Oliver, "Growth and Applications of T.B. Bronze Family Crystals," presented at the Southwest Optics Symposium, Albuquerque, NM, March 2-8, 1985.



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3. G.A. Rakuljic, A. Yariv, and R.R. Neurgaonkar, "A Comparative Evaluation of the Photorefractive Effect in  $\text{Sr}_{.6}\text{Ba}_{.4}\text{Nb}_2\text{O}_6$  (SBN) SBN:Fe, and SBN:Ce by Two-Beam Coupling," (1984).
4. G.A. Rakuljic, A. Yariv, and R.R. Neurgaonkar, "Application of the Band Transport Model to Photorefractive Strontium Barium Niobate," (1984).
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## APPENDIX

### A PHENOMENOLOGICAL ANALYSIS OF TETRAGONAL TUNGSTEN BRONZE FERROELECTRICS

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## ABSTRACT

A simple Devonshire form has been derived for the Phenomenological Elastic Gibbs Function to describe the elasto-dielectric parameters of simple proper ferroelectrics in the tungsten bronze structure family which has  $4/mmm$  prototypic point symmetry. For the assumption that all temperature dependence is carried by the Curie-Weiss behavior implicit in the quadratic term and that the expansion may be terminated at the first 6th order term, reasonable agreement between calculated and derived  $P_S$  vs.  $T$  curves in the ferroelectric phase can be obtained for a wide range of bronze compositions.

From the fitting it is clear that second and sixth rank terms are remarkably constant over a very wide range of bronze compositions. Variation in the negative fourth rank term is larger, but this is to be expected since it contains large contributions from electrostrictive and elastic terms which will depend upon boundary conditions.

These initial studies suggest that the phenomenological method may be used to derive expectation values for tensor parameters across the whole family of ferroelectric bronzes. The study also points up the need for more careful detailed studies of lattice strain, birefringence and permittivity as a function of temperature in model bronze compounds to provide more detailed checks of the method.



## 1.0 INTRODUCTION

The tungsten bronze family of simple proper ferroelectrics incorporates now almost 100 different end member compositions, most of which are mutually compatible in solid solution, so that an immense range of possible ferroelectrics is now available. In attempting to select compositions for device application in optics, nonlinear optics, electro-optics, acousto-optics, SAW, etc., it is important for each device to maximize a different combination of the tensor properties of the crystal, so that some theoretical predictive capability would be of major help in making rational choices in this bewildering range of possible bronze compositions. For complex structures like the ferroelectric bronzes, however, where different cations can have different fractional occupancy on several sites in the structure, a rigorous atomistic theory is, at present, out of the question. It is our purpose to explore the extent to which thermodynamic phenomenological methods can be used to correlate the tensor properties, point up the inadequacies of present experimental data, and suggest a more systematic experimental approach.

A rather simple Landau:Ginsburgh:Devonshire function for the Elastic Gibbs Free Energy of simple proper ferroelectric bronzes which can be derived for the 4/mmm prototype symmetry has been discussed earlier (1), and the function was used with good results to fit the dielectric, electric and piezoelectric properties of the  $\text{Sr}_{0.60}\text{Ba}_{0.40}\text{Nb}_2\text{O}_6$  (SBN:60) ferroelectric composition (2). A simple power series expansion up to the first 6th power terms in polarization, but including only fourth rank terms in elastic and elasto-electric coupling terms, proved adequate to explain dielectric, piezoelectric and spontaneous shape change data; however, it was necessary to include sixth order electrostriction to model the elastic constant behavior. The relaxor dielectric character of SBN was taken into account by using a narrow distribution of Curie temperatures  $T_c$ , and did not obtrude in the fitting process except for properties very close to  $\bar{T}_c$  where fluctuations in the polarization take  $\bar{P}_3^2$  far from zero (3).



## 2.0 THERMODYNAMIC PHENOMENOLOGY

Recapitulating our earlier studies, it has been the contention that an empirical thermodynamic elastic Gibbs function can be developed which will describe the polarization induced changes in the dielectric, elastic, thermal, piezoelectric and electro-optic properties in all possible simple proper ferroelectric phases of the tungsten bronze structure ferroelectrics.

Under the symmetry constraints of the 4/mm point symmetry for the prototypic form of the bronzes, the permitted dielectric stiffnesses  $\alpha_{ij}$ , fourth order stiffnesses  $\alpha_{ijkl}$ , electrostriction constants  $Q_{ijkl}$ , elastic compliances  $s_{ijkl}$ , and sixth order dielectric stiffnesses  $\alpha_{ijklmn}$  are listed in Tables I through IV.

Using the reduced notation 11  $\rightarrow$  1, 22  $\rightarrow$  2, 33  $\rightarrow$  3, 23 or 32  $\rightarrow$  4, 13 or 31  $\rightarrow$  5 and 12 or 21  $\rightarrow$  6 the elastic Gibbs function takes the form

$$\begin{aligned} \Delta G_1 = & \alpha_1(P_1^2 + P_2^2) + \alpha_3 P_3^2 + \alpha_{11}(P_1^4 + P_2^4) + \alpha_{33} P_3^4 \\ & + \alpha_{13}(P_1^2 P_3^2 + P_2^2 P_3^2) + \alpha_{12} P_1^2 P_2^2 + \alpha_{333} P_3^6 \\ & + \alpha_{111}(P_1^6 + P_2^6) - \frac{1}{2} s_{11}(X_1^2 + X_2^2) - s_{12} X_1 X_2 \\ & - s_{13}(X_1 + X_2) X_3 - \frac{1}{2} s_{33} X_3^2 - \frac{1}{2} s_{44}(X_4^2 + X_5^2) \\ & - \frac{1}{2} s_{66} X_6^2 - Q_{11}(P_1^2 X_1 + P_2^2 X_2) - Q_{12}(P_1^2 X_2 + P_2^2 X_1) \\ & - Q_{13}(P_1^2 X_3 + P_2^2 X_3) - Q_{31}(P_3^2 X_1 + P_3^2 X_2) \\ & - Q_{33} P_3^2 X_3 - Q_{44}(P_2 P_3 X_4 + P_1 P_3 X_5) \\ & - Q_{66} P_1 P_2 X_6 \end{aligned} \quad (1)$$



The first partial derivatives with respect to the polarization give the field components

$$\begin{aligned}\frac{\partial \Delta G}{\partial P_1} = & E_1 - 2a_1P_1 + 4a_{11}P_1^3 + 2a_{13}P_1P_3^2 \\ & + 2a_{12}P_1P_2^2 + 6a_{111}P_1^5 \\ & + Q_{13}P_1X_3 + Q_{44}P_3X_5 + Q_{66}P_1X_6\end{aligned}\quad (2)$$

$$\begin{aligned}\frac{\partial \Delta G}{\partial P_2} = & E_2 - 2a_1P_2 + 4a_{11}P_2^3 + 2a_{13}P_2P_3^2 \\ & + 2a_{12}P_2P_1^2 + 6a_{111}P_2^5 \\ & + 2Q_{13}P_2X_3 + Q_{44}P_3X_4 + Q_{66}P_1X_6\end{aligned}\quad (3)$$

$$\begin{aligned}\frac{\partial \Delta G}{\partial P_3} = & E_3 - 2a_3P_3 + 4a_{33}P_3^3 + 2a_{13}(P_1^2 + P_2^2)P_3 \\ & + 6a_{33}P_3^5 + 2Q_{31}P_3(X_1 + X_2) \\ & + 2Q_{33}P_3X_3 + Q_{44}(P_2X_4 + P_1X_5)\end{aligned}\quad (4)$$

It is the solutions of these equations with  $E_i = 0$  which determine the ferroelectric states for a free crystal ( $X = 0$ ). In general, there are seven possible ferroelectric species which can occur from the prototypic 4/mmm symmetry of the paraelectric phase of the tungsten bronze, each of which corresponds to a different combination of non-zero (spontaneous) values of the  $P_i$  components. All possible solutions for the three equations (2-4) were derived and reported by Cross and Pohanka (1968). Practically, however, just two of these solutions encompass all presently known simple ferroelectric bronzes. These are



$$(a) P_3^2 \neq 0 \quad P_1 = P_2 = 0$$

$$(b) P_1^2 = P_2^2 \neq 0 \quad P_3 = 0.$$

The species (a) corresponds to the Shuvalov (1970) species 4/mmm (1) D4 F4mm, where 4/mmm is the high temperature prototype point group and F4mm means that the crystal is ferroelectric of point group 4mm below the transition temperature. D(4) indicates that the spontaneous polarization  $P_s$  has definite orientation along the four-fold symmetry axes, and (1) denotes number of equivalent four-fold axes which is one. In other words, there are two domains of opposite orientation of  $P_s$  (I.E., 180° domains) along the four-fold prototypic axis. The second species (b) is one of the subtypes of 4/mmm (2) D2 Fmm2 with  $P_s$  along the two-fold axis which make angles of 45° with the 1 and 2 prototype axis ( $P_1^2 = P_2^2$ ) and has four equivalent ferroelectric domain states.

Substituting the conditions (a) into the general equations (2-4) gives the following conditions for stability:

$$P_1 = P_2 = 0 \quad 0 = 2a_3 + 4a_{33}P_3^2 + 6a_{333}P_3^4 \quad (5)$$

The isothermal dielectric stiffness  $\chi$  are

$$\begin{aligned} \chi_{11}^T &= 2a_1 + 2a_{13}P_3^2 \\ \chi_{22}^T &= 2a_1 + 2a_{13}P_3^2 \\ \chi_{33}^T &= 2a_3 + 12a_{33}P_3^2 + 30a_{333}P_3^4 \\ \chi_{12}^T &= \chi_{13}^T = \chi_{23}^T = 0 \end{aligned} \quad (6)$$

The tetragonal spontaneous strains are given by

$$\begin{aligned} x_1 &= Q_{31}P_3^2 & x_4 &= x_5 + x_6 = 0 \\ x_2 &= Q_{31}P_3^2 \\ x_3 &= Q_{33}P_3^2 \end{aligned} \quad (7)$$



and the piezoelectric b coefficients by

$$\begin{array}{lll}
 b_{11} = 0 & b_{21} = 0 & b_{31} = 2Q_{31}P_3 \\
 b_{12} = 0 & b_{22} = 0 & b_{32} = 2Q_{31}P_3 \\
 b_{13} = 0 & b_{23} = 0 & b_{33} = 2Q_{33}P_3 \\
 b_{14} = 0 & b_{24} = Q_{44}P_3 & b_{44} = 0 \\
 b_{15} = Q_{44}P_3 & b_{25} = 0 & b_{35} = 0 \\
 b_{16} = 0 & b_{26} = 0 & b_{36} = 0
 \end{array} \tag{8}$$

For the case (b) the corresponding equations take the form, for the stability conditions,

$$\begin{array}{l}
 P_1^2 = P_2^2 \quad 0 = 2a_1 + (4a_{11} + 2a_{12})P_1^2 + 6a_{111}P_1^4 \\
 P_3 = 0
 \end{array} \tag{9}$$

The isothermal stiffnesses are

$$\begin{array}{l}
 \chi_{11}^T = 2a_1 + 12a_{11}P_1^2 + 2a_{12}P_1^2 + 30a_{111}P_1^4 \\
 \chi_{22}^T = 2a_1 + 12a_{11}P_1^2 + 2a_{12}P_1^2 + 30a_{111}P_1^4 \\
 \chi_{33}^T = 2a_3 + 4a_{13}P_1^2 \\
 \chi_{34}^T = 4a_{12}P_1^2 \quad \chi_{13} = \chi_{23} = 0
 \end{array} \tag{10}$$

It may be noted that the coefficients here are expressed with respect to the original prototypic axes and thus satisfy pseudomonoclinic symmetry. However, a simple rotation of the matrix by 45° in the 1, 2 plane would reveal the true orthorhombic symmetry.





Spontaneous elastic strains take the form

$$\begin{aligned}x_1 &= (Q_{11}+Q_{12})P_1^2 \\x_2 &= (Q_{11}+Q_{12})P_1^2 \\x_3 &= 2Q_{13}P_1^2 \\x_6 &= Q_{66}P_1^2 \quad x_4 = x_5 = 0\end{aligned}\tag{11}$$

and the piezoelectric coefficients are

$$\begin{aligned}b_{11} &= 2Q_{11}P_1 & b_{21} &= 2Q_{12}P_1 & b_{31} &= 0 \\b_{12} &= 2Q_{12}P_1 & b_{22} &= 2Q_{11}P_1 & b_{32} &= 0 \\b_{13} &= 2Q_{13}P_1 & b_{23} &= 2Q_{13}P_1 & b_{33} &= 0 \\b_{14} &= 0 & b_{24} &= 0 & b_{34} &= Q_{44}P_1 \\b_{15} &= 0 & b_{25} &= 0 & b_{35} &= Q_{44}P_1 \\b_{16} &= Q_{66}P_1 & b_{26} &= Q_{66}P_1 & b_{36} &= 0\end{aligned}\tag{12}$$



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Table I  
Equivalent Second and Fourth Rank Dielectric Terms for 4/ $\infty$  Symmetry

Nye's Matrix Notation		Full Tensor Notation		Number of Equivalent Terms
Term	Symmetry Equivalent Terms	Term	Symmetry Equivalent Terms	
$\alpha_1$	$\alpha_2$	$\alpha_{11}$	$\alpha_{22}$	2
$\alpha_3$		$\alpha_{33}$		1
$\alpha_{11}$	$\alpha_{22}$	$\alpha_{1111}$	$\alpha_{2222}$	2
$\alpha_{12}$	$\alpha_{21}, \alpha_{66}$	$\alpha_{1122}$	$\alpha_{1212}, \alpha_{1221}, \alpha_{2112}, \alpha_{2121}, \alpha_{2211}$	
$\alpha_{13}$	$\alpha_{31}, \alpha_{23}, \alpha_{32}, \alpha_{44}, \alpha_{55}$ ( $\alpha_{44} = 4\alpha_{2323}$ )	$\alpha_{1133}$	$\alpha_{3311}, \alpha_{2233}, \alpha_{1313}, \alpha_{1313}, \alpha_{1331}, \alpha_{3113}, \alpha_{3131}, \alpha_{2323}, \alpha_{2332}, \alpha_{3223}, \alpha_{3232}$	12
$\alpha_{33}$		$\alpha_{3333}$		1



Table II  
Equivalent Electrostriction Terms for 4/mm Symmetry

Nye's Matrix Notation			Full Tensor Notation		Number of Equivalent Terms
Term	Symmetry	Equivalent Terms	Term	Symmetry Equivalent Terms	
$Q_{11}$	$Q_{22}$		$Q_{1111}$	$Q_{2222}$	2
$Q_{12}$	$Q_{21}$		$Q_{1122}$	$Q_{2211}$	2
$Q_{13}$	$Q_{23}$		$Q_{1133}$	$Q_{2233}$	2
$Q_{31}$	$Q_{32}$		$Q_{3311}$	$Q_{3322}$	2
$Q_{33}$			$Q_{3333}$		1
$Q_{44}$	$Q_{45}$		$Q_{2323}$	$Q_{2332}, Q_{3223}, Q_{3232},$ $Q_{1313}, Q_{1331}, Q_{8113},$ $Q_{3151}$	8
$Q_{66}$			$Q_{1212}$	$Q_{1221}, Q_{2112}, Q_{2121}$	4



Table III  
Equivalent Elastic Compliance Terms for 4/mmm Symmetry

Nye's Matrix Notation			Full Tensor Notation		Number of Equivalent Terms
Term	Symmetry	Equivalent Terms	Term	Symmetry Equivalent Terms	
$s_{11}$	$s_{22}$		$s_{1111}$	$s_{2222}$	2
$s_{12}$	$s_{21}$		$s_{1122}$	$s_{2211}$	2
$s_{13}$	$s_{31}, s_{23}, s_{32}$		$s_{1133}$	$s_{3311}, s_{2233}, s_{3322}$	4
$s_{33}$			$s_{3333}$		1
$s_{44}$	$s_{55}$		$s_{2323}$	$s_{2332}, s_{3223}, s_{3232},$ $s_{1313}, s_{1331}, s_{3113},$ $s_{3131}$	8
$s_{66}$			$s_{1212}$	$s_{1221}, s_{2112}, s_{2121}$	4



Table IV  
Equivalent Sixth Rank Tensor Terms of the Form  $\alpha(P^6)$   
for  $4/\bar{mmm}$  Symmetry

Term	Symmetry Related Terms	Number of Equivalent Terms
1. $\alpha_{111}$	222	2
2. $\alpha_{112}$	166, 121, 616, 661, 211, 221, 266, 212, 626, 662, 122	30
3. $\alpha_{113}$	155, 131, 515, 551, 331, 223, 244, 232, 424, 442, 322	30
4. $\alpha_{123}$	144, 132, 525, 645, 546, 636, 663, 564, 654, 552, 321, 441, 231, 465, 366, 255, 456, 213, 414, 312	90
5. $\alpha_{133}$	535, 553, 331, 355, 313, 233, 434, 443, 332, 344, 323	30
6. $\alpha_{333}$		1



### 3.0 POTENTIAL UTILITY OF THE PHENOMENOLOGICAL THEORY

#### 3.1 Introduction

It is evident from Tables I through IV that a substantial number of constants are required to characterize the bronzes in this phenomenological manner. The only formal benefit is that all the elasto-dielectric parameters of the lower symmetry ferroelectric forms can be characterized in terms of the nonlinear parameters of the higher symmetry prototype form.

In principle, it is possible that all the parameters can be functions of both temperature and composition. However, several pieces of evidence, both direct and indirect suggest that:

- (a) The dominant temperature dependence is carried in the terms  $\alpha_1$  and  $\alpha_3$  which have a Curie-Weiss form

$$\begin{aligned}\alpha_1 &= \alpha_{10} (T - \theta_1) \\ \alpha_3 &= \alpha_{30} (T - \theta_3)\end{aligned}\tag{13}$$

- (b) The higher order constants do not change markedly with either temperature or composition across a wide field of compounds and solid solutions with the bronze structure.

In earlier studies we have demonstrated

1. That in all known ferroelectric bronzes, only two of the seven possible ferroelectric species which are available from the 4/mmm prototype occur in nature.
2. In the tetragonal ferroelectric form in  $(\text{Sr}_{0.61}\text{Ba}_{0.39})\text{Nb}_2\text{O}_6$ , which is the congruently melting SBN composition, the data followed very closely to the phenomenology except for temperatures close to the Curie point  $T_c$ , and all parameters have been evaluated.



3. For the  $(\text{Pb}_{1-x}\text{Ba}_x)\text{Nb}_2\text{O}_6$  compositions in the tetragonal phase field, but close to the morphotropic phase boundary at the  $(\text{Pb}_{0.6}\text{Ba}_{0.4})\text{Nb}_2\text{O}_6$  composition, the dielectric, piezoelectric and electro-optic behavior can be quite accurately modeled using the phenomenological constants for SBN and just adjusting  $\Theta_1$  and  $Q_3$  to conform to the observed Curie-Weiss behavior in these compositions.<sup>4</sup>

The success to date with the modeling suggest that we attempt a more ambitious assessment of the range of validity of our simple hypotheses (a) and (b) above using a much wider range of bronze compounds and making use of literature values to evaluate directly, wherever possible, the stiffness parameters. The results of this effort will form the bulk of this paper.

A second feature which has become evident from our modeling of the tungsten bronze ferroelectrics is that particularly in the elastic response, the relaxor character of the bronzes is reflected in a breakdown of the static phenomenological model at temperatures close to  $T_c$  due to the onset of fluctuations in  $P$ . Thus for a range of temperatures above  $T_c$ , it is evident that even though  $\bar{P} = 0$ , it is rigorously true that  $\bar{P}^2 \neq 0$ . The onset of a substantial fluctuating component in  $P$  will clearly affect all parameters which depend on even powers of  $P$ , such as the linear dimensions, since

$$x_{1j} = Q_{1j33}P_3^2 \quad (14)$$

as well as the optical refractive index given by

$$\Delta B_{1j} = g_{1j33}P_3^2 \quad (15)$$

and the elastic compliance

$$s_{1jkl} = \phi_{1jkl33}P_3^2 \quad (16)$$

Perhaps the easiest to analyze is the strain response, and this will be the subject of a subsequent paper.



### 3.2 Evaluation of the Thermodynamic Parameters

In spite of the fact that more than 100 different ferroelectric compounds with the tungsten bronze structure have been synthesized, and innumerable solid solutions can be made between these end member compositions, there is a genuine paucity of reliable experimental data from which to evaluate the thermodynamic constants. For many materials, only ceramic samples have been made and in these, it is impossible to separate the individual tensor components. Even in many systems where good single crystals have been grown, the headlong rush to print has left many of the important parameters unmeasured.

For this study we have been able to find adequate but incomplete data for several  $\text{Sr}_{1-x}\text{Ba}_x\text{Nb}_2\text{O}_6$  solid solutions. In several  $\text{La}_2\text{O}_3:\text{Sr}_2\text{KNb}_5\text{O}_{15}$  compounds and solid solutions and for pure  $\text{Sr}_2\text{KNb}_5\text{O}_{15}$  there are also adequate, though incomplete, data.  $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$  may be analysed on this model if the weak ferroelastic phase change near  $370^\circ\text{C}$  is neglected, and there are some data for a titanium modified  $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$ . Similarly, in  $\text{K}_3\text{Li}_2\text{Nb}_5\text{O}_{15}$  there are adequate data for some of the constants, though the transverse dielectric response has apparently not been measured.

In the orthorhombic ferroelectric form, we have only been able to find data for  $\text{PbNb}_2\text{O}_6$  and for  $\text{Pb}_2\text{KNb}_5\text{O}_{15}$ . The fitting to obtain the thermodynamic parameters is, however, more difficult in these compositions and will be covered in a subsequent paper.

For the tetragonal ferroelectric form, the evaluation is relatively straight-forward. The constant  $\alpha_3$  has the form  $\alpha_3 = \alpha_{30}(T-\theta_3)$  which leads to an equation for the stiffness  $x_{33}$  above  $T_c$  of the form

$$x_{33} = 2\alpha_{30}(T-\theta_3) \quad (17)$$

Thus the extrapolation of the Curie Weiss plot of stiffness above  $T_c$  gives the temperature  $\theta$  and the slope in the constant  $2\alpha_{30}$ .





By equating the  $\Delta G$  values in ferroelectric and paraelectric states at  $T_c$ , the equation for  $P_s$  can be put into the Devonshire form

$$\frac{T-\theta}{T_c-\theta} - 4\left(\frac{P_3}{P_{30}}\right)^2 + 3\left(\frac{P_3}{P_{30}}\right)^4 = 0 \quad (18)$$

in which  $T_c - \theta$  and  $P_{30}$  are the only fitting parameters. Often, unfortunately, the published  $P_s$  vs  $T$  data for ferroelectric crystals is unreliable, particularly at temperatures remote from  $T_c$  where it is often difficult to pole to a single domain state. Thus it is wise to check the shape of the polarization function by using a less direct method, e.g. the spontaneous strains  $\Delta c/c$  and  $\Delta a/a$  induced in the ferroelectric form are electrostrictive in nature and thus scale with  $P_s^2$ . The piezoelectric  $b_{ij}$  constants on the other hand, being morphic, scale directly with  $P_s$  as do the linear electro-optic effect and the nonlinear Miller  $\delta$  coefficients.

A typical fitting of the different  $P_s$  data for  $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$  is shown in Fig. 1. Clearly the Devonshire form is in excellent agreement with the 'birefringence' data which are probably most reliable in this crystal. From the values of  $T_c$ ,  $\theta$ ,  $P_{30}$  and  $\chi_{30}$ , the  $\alpha$  constants are given by

$$\alpha_3 = 1/2 \alpha_{30}(T_c - \theta_3) \quad (19)$$

$$\alpha_{33} = - \frac{\alpha_{30}(T_c - \theta_3)}{P_{30}} \quad (20)$$

$$\alpha_{333} = \frac{\alpha_{30}(T_c - \theta_3)}{2(P_{30})^4} \quad (21)$$

For the constant  $\alpha_1$  and  $\alpha_{13}$ , dielectric data for a section parallel to the  $c$  axis ( $\epsilon_a$ ) is required. Above  $T_c$ ,



so that  $2\alpha_{10}$  is the Curie-Weiss slope and  $\Theta_1$  is the extrapolated Curie temperature.

To derive  $\alpha_{13}$  it is then a simple matter to make use of equation (10) to obtain, by the least squares method, a best fit to the experimental data below  $T_c$ , taking now calculated values for  $P_3$  vs  $T$ . A typical plot comparing measured and calculated values for  $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$  is given in Fig. 2. Using these methods, constants for the bronze compositions derived are listed in Table V.

### 3.3 Discussion

It may be noted at once that for  $\alpha_{30}$  and  $\alpha_{333}$  there is excellent agreement over a very wide range of bronze compositions. The constant  $\alpha_{10}$  is also within a narrow range, though here the stiffness is much larger and the Curie-Weiss slope more difficult to read precisely. The  $\alpha_{33}$  values cover a wider range and this also is perhaps not surprising. In the elastic Gibbs function, the negative value of  $\alpha_{33}$  comes about because of a strong contribution from elastic and electrostrictive constants in the free crystal. Thus the magnitude of  $\alpha_{33}$  is markedly dependent on the elastic boundary conditions and probably therefore on the crystal perfection. The  $\alpha_{13}$  values also cover a rather wider range, but here the error is probably in the evaluation.

In summary, it does appear from these preliminary data that the original hypothesis of a constancy of the higher order stiffnesses is a good approximation for the tetragonal bronze ferroelectrics, and thus can form a basis for the analysis of the properties of a very wide range of bronze compositions.

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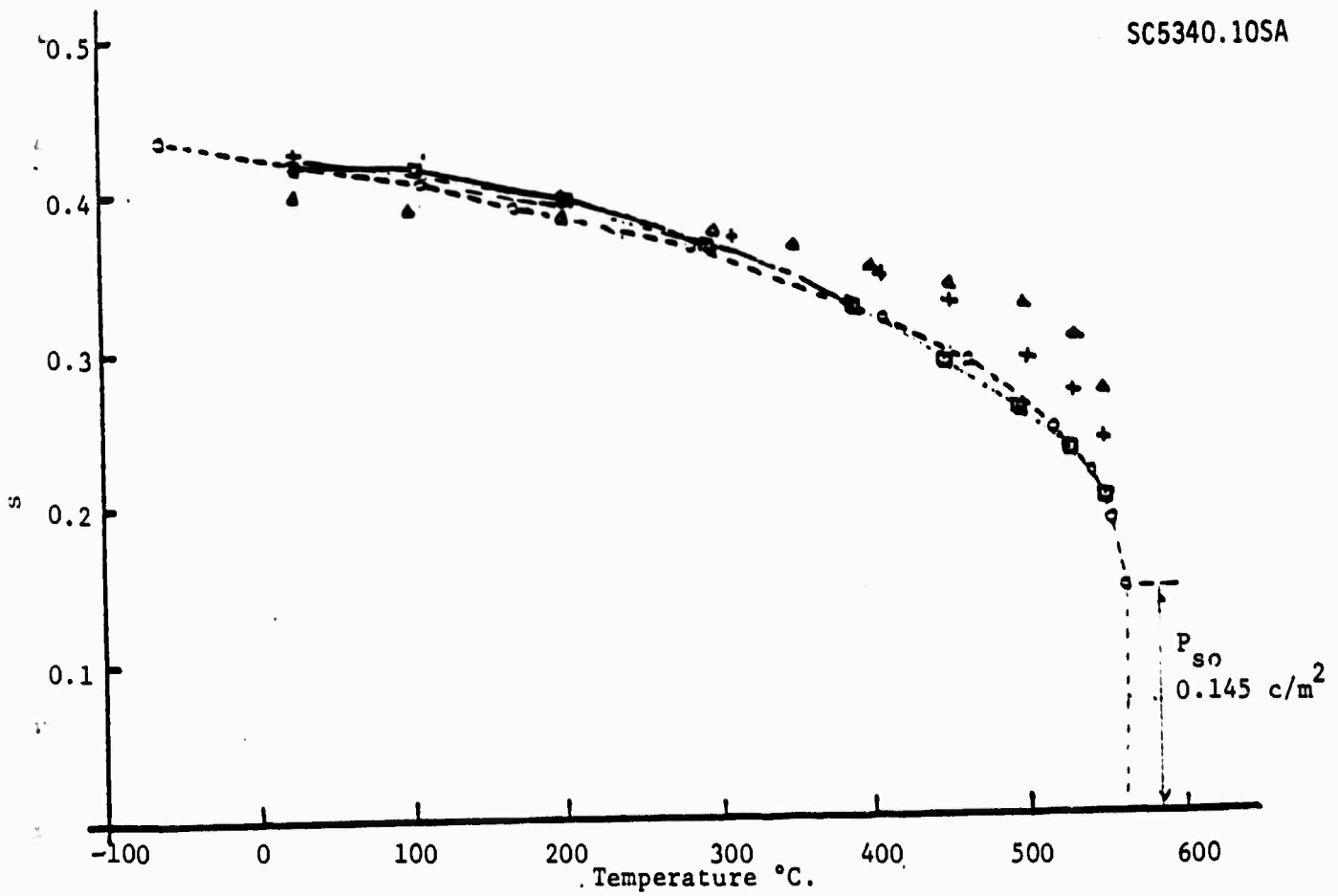


Figure 1. Phenomenological fitting of  $P_s$  vs  $T$  in  $\text{NaBa}_2\text{Nb}_5\text{O}_{15}$ .

o o o Phenomenology  
 $\Delta$   $\Delta$   $\Delta$  Nonlinear Optical Results  
+ + + Pyroelectric Measurement  
Optical Impermeability

$T_c = 563^\circ\text{C}$ .  
 $T_3 = 560^\circ\text{C}$ .  
 $P_{so} = 0.145 \text{ c/m}^2$ .



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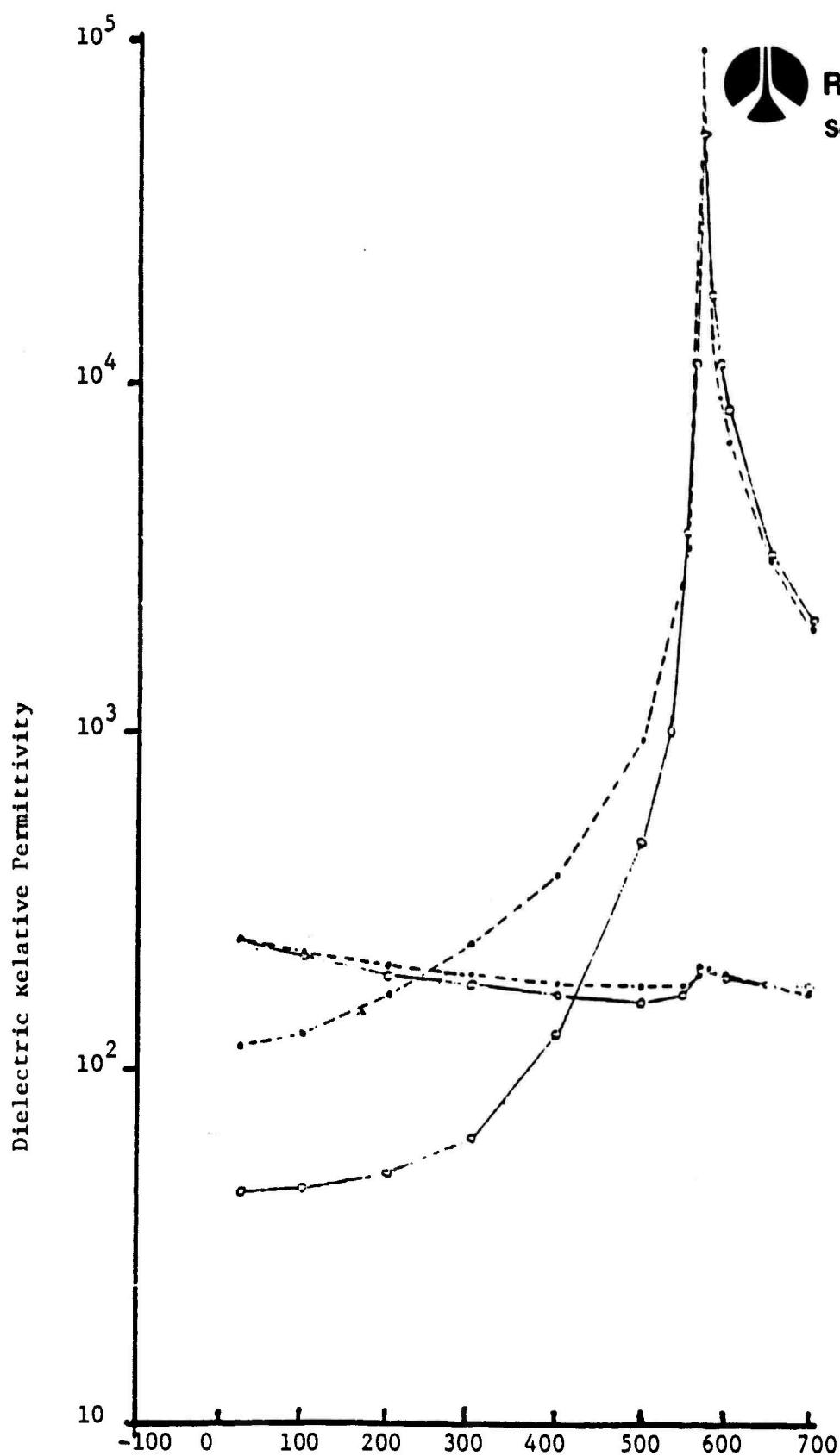


Figure 2. Phenomenological fitting to the dielectric permittivity in single crystal  $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$ .

. . . Theory.  
o o o Experiment.



Table V. Thermodynamic Constants for Tetragonal Tungsten Bronze Ferroelectric Crystals.

Compound	$1/2 \alpha_{30}$	$12 \alpha_{33}$	$30 \alpha_{333}$	$1/2 \alpha_{10}$	$\alpha_{13}$
$\text{Ba}_{0.75}\text{Sr}_{0.25}\text{Nb}_2\text{O}_6$	$2.4 \cdot 10^{-6}$	$-2.3 \cdot 10^{-3}$	$3.6 \cdot 10^{-1}$		
$\text{Ba}_{0.5}\text{Sr}_{0.5}\text{Nb}_2\text{O}_6$	$2.4 \cdot 10^{-6}$	$-6.2 \cdot 10^{-3}$	$3.2 \cdot 10^{-1}$		
$\text{Ba}_{0.4}\text{Sr}_{0.6}\text{Nb}_2\text{O}_6$	$1.6 \cdot 10^{-6}$	$-11.0 \cdot 10^{-3}$	$3.6 \cdot 10^{-1}$		
$\text{Ba}_{0.33}\text{Sr}_{0.67}\text{Nb}_2\text{O}_6$	$2.7 \cdot 10^{-6}$	$-1.6 \cdot 10^{-3}$	$3.1 \cdot 10^{-1}$		
$\text{Ba}_{0.39}\text{Sr}_{0.61}\text{Nb}_2\text{O}_6$	$2.52 \cdot 10^{-6}$	$-8.4 \cdot 10^{-3}$	$3.6 \cdot 10^{-1}$	$3.73 \cdot 10^{-6}$	$2.1 \cdot 10^{-3}$
$\text{KSr}_2\text{Nb}_5\text{O}_{15}$	$3.45 \cdot 10^{-6}$	$-9.7 \cdot 10^{-3}$	$3.4 \cdot 10^{-1}$	$2.4 \cdot 10^{-6}$	$11.3 \cdot 10^{-3}$
3% (La) $\text{KSr}_2\text{Nb}_5\text{O}_{15}$	$2.2 \cdot 10^{-6}$	$-9.6 \cdot 10^{-3}$	$2.85 \cdot 10^{-1}$		
6% (La) $\text{KSr}_2\text{Nb}_5\text{O}_{15}$	$2.0 \cdot 10^{-6}$	$-10.5 \cdot 10^{-3}$	$3.8 \cdot 10^{-1}$		
9% (La) $\text{KSr}_2\text{Nb}_5\text{O}_{15}$	$3.14 \cdot 10^{-6}$	$-12.2 \cdot 10^{-3}$	$3.58 \cdot 10^{-1}$		
$\text{NaB}_2\text{Nb}_5\text{O}_{15}$	$3.44 \cdot 10^{-6}$	$-11.46 \cdot 10^{-3}$	$2.5 \cdot 10^{-1}$	$5.15 \cdot 10^{-6}$	$13.3 \cdot 10^{-3}$
$\text{Na}_{1.6}\text{Ba}_{4.35}\text{Nb}_{9.65}\text{Ti}_{0.35}\text{O}_{30}$	$3.56 \cdot 10^{-6}$	$-5.34 \cdot 10^{-3}$	$1.63 \cdot 10^{-1}$		
$\text{K}_3\text{Li}_2\text{Nb}_5\text{O}_{15}$	$2.87 \cdot 10^{-6}$	$-14.16 \cdot 10^{-3}$	$1.13 \cdot 10^{-1}$	$2.82 \cdot 10^{-6}$	



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